

## Advancement of Integral Fast Reactor

Asif Ali Maitlo <sup>a,\*</sup>, Waleed Raza <sup>b</sup>, Muhammad Nazim Lakhan <sup>c</sup>, Amir Ali <sup>b</sup>, Abdul Hanan <sup>c</sup>, Sajid Hussain <sup>a</sup>, Kishore Chand <sup>c</sup>, Vinod Kumar <sup>a</sup>

<sup>a</sup>Fundamental Science on Nuclear Safety and Simulation Technology Laboratory, Harbin Engineering University, PR China

<sup>b</sup>College of Underwater Acoustic Engineering, Harbin Engineering University, PR, China

<sup>c</sup>College of Materials Science and Chemical Engineering, Harbin Engineering University, PR China

**Abstract--** In this paper, the advancement of the integral fast reactor (IFR) is studied. We proposed the safety passive inherent approach which keeps the IFR operations safe from the maintenance cost. Additionally, it is observed that when failure appears in the reactor then safety passive inherent works efficiently and it turns off the reactor to preserve the safety. Therefore, it is necessary to use the inherent properties of the metallic fuel such as liquid metal, and it should be cooled in a way to substantial developments in the total appearances of the reactor system. Moreover, the key advantages of the IFR concept are narrated briefly with its mechanic position and the future development and research directions.

**Keywords:-** Integrated fast reactor, Safety passive inherent, Sodium liquid metal, Economics

Date Received 04-11-2020

Date Accepted 16-11-2020

Date Published 18-12-2020

### I. INTRODUCTION

The concept of the integral fast reactor (IFR) was evolved by the Argonne National Laboratory for novel ideas of the reactor to the coming generation. Recently, the liquid metal sodium (LMS) has attracted a lot of attention owing to its usage as a primary coolant in an advanced type of nuclear reactor named as liquid metal fast reactor (LMFR) and has been used as IFR [1]. The most attractive specific property of fluid metal cooling is the climatic conditions in the main reactor system. The main operation of LMS is to cool the nuclear reactors for electricity generation [2]. In U.S patent No 4,508,677, liquid metal cooled reactors (LMCR) showed numerous advantages by utilizing sodium or sodium-potassium coolant [3]. Water-cooled reactors usually work at or near the boiling point of water. Temperature rise can result in steam generation and increased pressure. Sodium or sodium-potassium exhibits a high boiling point in the range of 1800°F at 1 atmospheric pressure. The normal operating temperature of the reactor is in the range of 900°F. The heating capacity of liquid metal (LM) allows the sodium or sodium-potassium to be heated at higher than 100°F without materials danger failure in the reactor [4]. In previous years, a lot of research has been carried out in the U.S on various kinds of liquid metal reactors (LMR's). Another key role of the IFR idea is the metallic fuel (MF) which has shown an exceptional development and metallic fuel-based IFR emerged up as a promising choice [5]. The first specific electric power was produced by the experimental breeding Reactor-I (EBR-I) at Argonne West in Idaho (U.S) and expired in August 1951. EBR-1 produced the 1.2 (MWT) megawatt thermal power and applied the highest uranium metal fuel alloy clad along the 347 SS was cooled by sodium-potassium NaK. The

first produced electricity by EBR-1 reactor was 4 light bulbs which proved that the reactivity coefficients such as coolant metallic fuels were the main feature of fast reactors [6]. There were created 4 cores in the EBR-I; In the metal core of EBR-I had partial flame up; as proof, several successive LMRS were made to used oxide fuel basic on the expertise with light water reactors (LWRs). The EBR-I reactor was expired at the end of 1963 due to the three methods to shut down or deduce the power of the reactor. The first one was due to take way the control rods; this was the slowest method and more-mild for the decrease in the reactor power. The second one was the emitting of the safety rod due to the 'reactor off' button, this was usually brought the whole shut down the reactor accessibly prepared for restart. The third scheme was all reactors shut down due to the pushing "reactor scram" [7, 8]. The EBR-II was established in December 1953 and it became operable in 1964 with the production of electricity around 62.5 MWT. Over time, the power was beginning to shut in 1994 due to the fuels and testing materials were shafted. This idea was completely explained in a sodium-cooled power plant breeder reactor with the reprocessing of metallic fuel. It was completely successful from 1964 to 1969 than (ceramic oxides and metal, carbides, and nitrides of plutonium and uranium) for the highest fast reactors [9]. The EBRs were significant to the US IFR program, which has the aim of improved completely integrated scheme with pyro-processing, fast reactor and fuel fabrication are complex due reactor shutdown problems. Therefore, it is a timely need to carry out the inherent safety measurements for metallic fuel reactors to ensure efficient productivity. Inherent passive safety is needed for new advance generation nuclear reactors. The passive nuclear safety doesn't need any vigorous involvement on the part of performance either electronic feedback, or electrical in direction to carry on the reactor to a safe state of shutdown, in the time-specific emergency [10]. Furthermore, the inherent passive safety can be beneficial for IFR by carrying out the desired operation smoothly which alternatively helps the reactor to increase the uranium resources

and gain large energy. The basic development of IFR consists of financial matters, waste administration, and safety passive inherent [11, 12].

In this paper, early researched integral fast reactors (IFR) reactors such as EBR-1 and EBR-2 have been discussed with their shutdown problems and IFR development concept such as liquid metal sodium (LMS) as coolant reactor has been investigated using of financial matters, waste administration, and inherent passive safety approach. Liquid metal cooled reactors (LMCR) can be affirmed as an efficient approach by carrying out safety passive inherent.

## II. SAFETY PASSIVE INHERENT

The main aim of safety passive inherent is to improve the safety and focus on the IFR design to achieve positive feedback and passive model for the cooling reactor to detect the accident initiators. The intrinsic scheme features sustain the balance between power creation and reactor cooling ability to avoid fuel failure in occurrences when the machine safety system fails [13]. This reporting feature hugely influences the selection of reactor material. The working condition of metallic fuel is usually better than normal oxide fuels and lead to a straight result. Inherent properties ensure the safety passive react in model-based accidents without anticipated transient scram and report the accidents either the normal working or local fault can be added to cladding failures [14]. The characteristic of inherent safety might be gained successfully by investigating the safety of the primary layout circuit and the physical properties of the core reactor. Sodium is only a single significant material of liquid metal reactor (LMR) which works at atmospheric-pressure in the main reactor system. The margin between sodium boiling temperature  $-900^{\circ}\text{C}$  and the cooling working temperature is ( $350^{\circ}\text{C}$  to  $510^{\circ}\text{C}$ ). The enlarge margin to boiling coolant temperature, much thermal act of the configuration pool reactor scheme, and including all properties of metal to deliver only one inherent passive safety [3]. However, the melting temperature of metallic fuel is poorer than the oxide fuel which alternatively depicts the huge difficulty to increase the fuel temperature due to the rich thermal conductivity (metal vs-2 W/mK for  $-20$  W/mK for oxide). Features of the inherent passive safety include the anticipated transient without scram (ATWS) occasion, loss of heat sink without scram (LOHSWS), and the loss of flow without scram (LOFWS). However, it is also observed that the coolant temperature rises as flow decreases quite early in the (LOFWS). Hence the rise in coolant temperature proved by the thermal expansion of the core [15]. The main vital factor which differentiates the LOHSWS and LOFWS feedback in oxide and among two fuels the difference in metal fuel at stored Doppler reactivity. The settled Doppler reactivity reveals back as an essential input as the power is decreased, attending to remove the drawback

because of the increase in coolant temperature [16, 17]. Thus, the force is decreased quickly. Interestingly, oxide fuel has a lot more preserved Doppler reactivity (fundamentally because of the higher fuel temperatures instead of the distinction in the Doppler coefficient itself), and the force doesn't diminish quickly during the LOFWS or LOHSWS occasion. At the point when the force has been decreased to rot power levels to counter the put-away Doppler reactivity, the coolant temperature keeps up a lot higher incentive in an oxide core. An ordinary examination of LOFWS between the metal and oxide is shown in Fig. 1

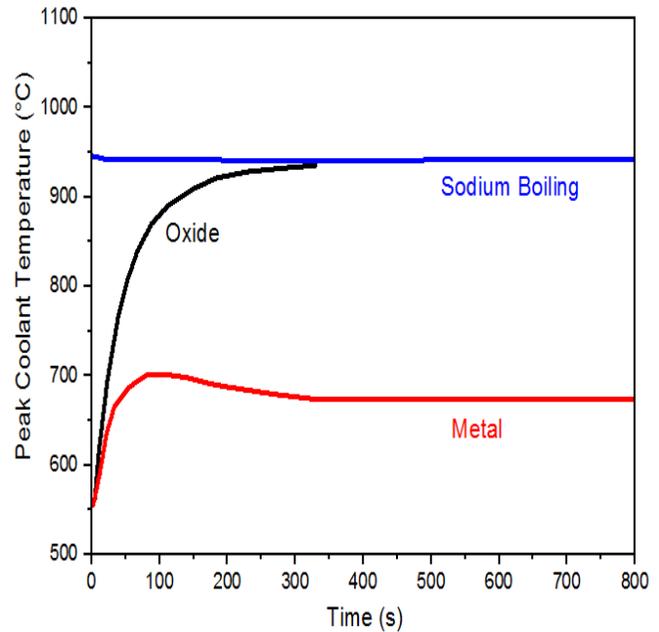


Figure 1 Comparison of metalcore and oxide responses to a loss of flow without scram (LOFWS) event for a typical large reactor

## III. FUEL PERFORMANCE

An integral fast reactor (IFR) idea has been generated as a model to depict the fuel performance. Metallic fuel is considered a better choice owing to its benefits such as easy to fabricate, excellent steady-state, and off-normal performance characteristics [18]. Metallic fuel slugs are usually produced through an injection casting approach with a size of 30 to 40 cm in length and 0.5 cm in diameter. In an individual cladding jacket, one to three fuel slugs are applied and a sodium bond was adopted to fill the discontinuity between slugs and cladding. The fuel slug cross-section area is determined as 75% of the accessible area in the cladding. The fission gas bubbles breed lead to the inducing fuel swelling as the fuel is irradiated. As the fuel expands out to the cladding divider, the splitting gas bubbles interconnect and give the plenum situated on the head of the fuel segment with a gas release path [19]. The key to preventing further fuel swelling and minimizing any major cladding stresses due to fuel/cladding touch is this interconnected porosity. It is depicted in Fig. 2 that metallic fuel exhibits a higher breeding ratio as compare with carbide or oxide fuels. The metallic fuel-based cores also exhibit higher breeding potential owing to a better neutron financial level

associated with the hardened spectrum. Further, it also allows IFR reactor centre plan upgrades, for example, limiting the reactivity swing over the working cycle, expanded cycle length, and so on.

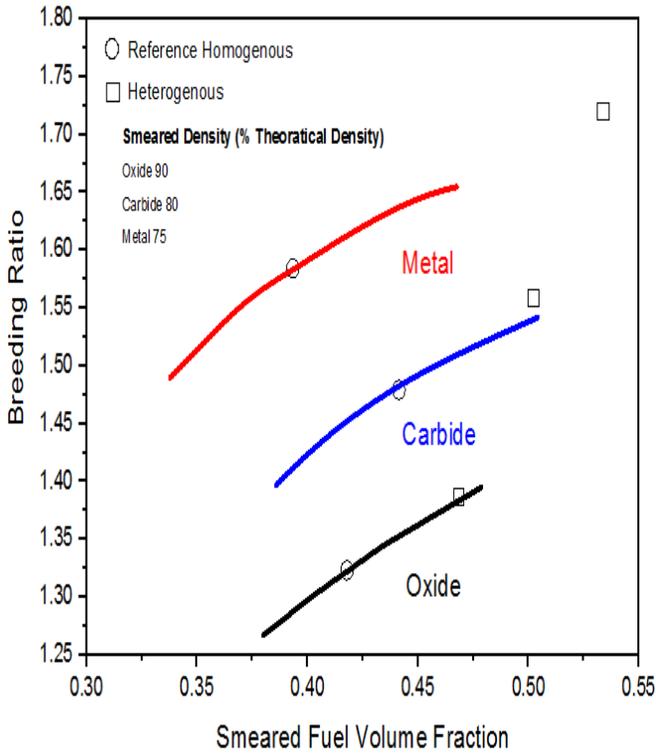


Figure 2 Comparison of breeding ratio potentials of metal-fuel, oxide, carbide.

#### IV. ECONOMICS

An assured calculation of the economic performance of IRF is not still sure. Recently, technology monitoring and market aspects have reformed IFR performance suggestively more than the 40 years since the economic calculation associated with the light water reactor (LWR) [20]. The economic effectiveness of the present reactor scheme is an essential condition for advanced reactors to cross through the commercial nuclear market. The modern nuclear reactor's economics is dominated by the fuel cycle cost and plant capital cost. LWR experience shows that much of the plant capital expense is correlated with the balance of plant (BOP) and backhanded costs, for example, field designing and development administrations [21]. The IFR concept offers an opportunity for the BOP to establish a newly built strategy that would deliver significant cost savings. Combined with favorable reactivity feedback properties of the metallic fuel, broad thermal inertia related to the sodium pool develop the reactor system to prevent different transients originating from the BOP [22]. The IFR concept also provides a dramatic decrease in fuel cycle cost as associated with the traditional Purex-based oxide fuel cycle. In the IFR fuel cycle, there are few steps and all the processes are extremely compact. In the three fields of reprocessing, production, and waste, there

Table 1 FS fast spectrum molten salt reactor (FS-MSR) economic Performance attributes and cost implications.

is room for drastic simplifications and cost cuts. IFR fuel cycle facility has a point by point calculated plan in light of the fact that the required fuel cycle office is so not quite the same as Purex-offices to give a firm specialized premise to measuring the IFR fuel cycle financial matters as depicted in the previous study. It should be noticed that the representations provided here are for deployment on a small scale. The cost favor of the IFR fuel cycle compared to the oxide is expected. If the level of the fuel cycle availability is scaled up, the fuel cycle dependent on Purex reprocessing would be decreased the fuel cycle size and facility. While conducting these both tests than the coolant temperature response quite early in Figures 3 and 4. Hence the EBR-II teste explained in a real way and what can be happened with metallic fuel and liquid metal cooling in obtaining wind-level by the safety passive inherent.

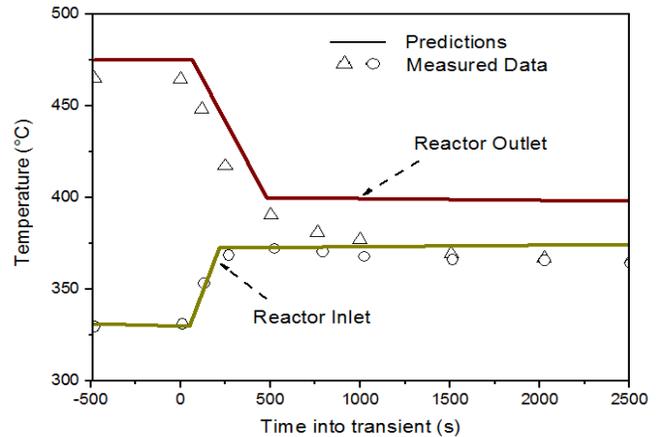


Figure 3 Loss of Flow without scram (LOFWS) test in Experimental Breeding Reactor (EBR-II).

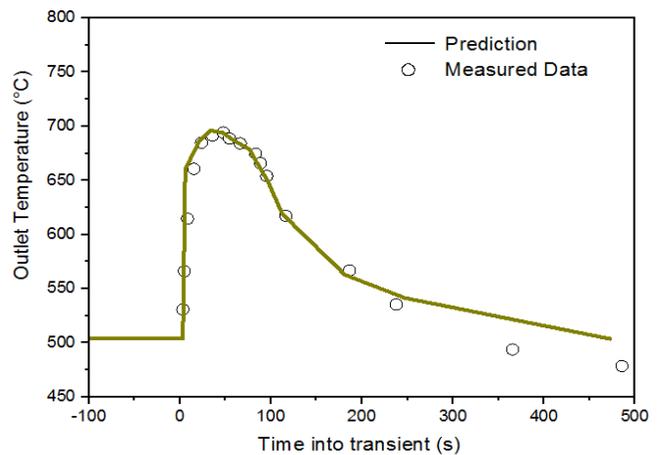


Figure 4 Loss of heat sink without scram (LOHSWS) test in Experimental Breeding reactor (EBR-II).

Difference relative to existing LWRs	Consequence	Effect on costs/revenues
<ul style="list-style-type: none"> <li>• Primary coolant</li> <li>• Homogenous liquid</li> <li>• fuel</li> </ul>	Higher primary coolant volumetric heat capacity	<ul style="list-style-type: none"> <li>• Lower capital cost for pipes, pumps</li> <li>• Heat exchange</li> </ul>
	No qualification, or fuel testing, qualification, or fabrication	<ul style="list-style-type: none"> <li>• Lower fuel acquisition cost</li> </ul>
	No cladding- or matrix-based temperature limits in an accident scenarios.	<ul style="list-style-type: none"> <li>• Lower capital cost for passive and simpler</li> <li>• Active reactor safety systems</li> <li>• Lower O&amp;M cost attributed to active reactor</li> <li>• Safety systems</li> </ul>
	No irradiated cladding or matrix the material in the ultimate waste stream	<ul style="list-style-type: none"> <li>• Lower disposal cost</li> <li>• Plant life</li> </ul>
	fission product barrier by No cladding	<ul style="list-style-type: none"> <li>• Potential higher capital cost for a replacement</li> <li>• Fission product barrier</li> </ul>
<ul style="list-style-type: none"> <li>• Online fuel</li> <li>• Processing</li> </ul>	No cladding-based burnup limits	<ul style="list-style-type: none"> <li>• Higher electricity generation revenue per unit</li> <li>• Mass and fuel</li> </ul>
	low-pressure, chemically stable coolant and visually transparent	<ul style="list-style-type: none"> <li>• Lower capital cost</li> <li>• Pipes Vessels Lower O&amp;</li> <li>• attributed to overall system maintenance</li> </ul>
	Flexible input fuel chemical	<ul style="list-style-type: none"> <li>• Potential lower fuel</li> <li>• Acquisition cost</li> <li>• Dependent on the market availability</li> </ul>
	Primary coolant chemistry Greater the control fuel	<ul style="list-style-type: none"> <li>• Salt treatment plant</li> <li>• Higher capital cost</li> </ul>
	Fissile-bearing Primary coolant and highly radioactive	<ul style="list-style-type: none"> <li>• Safe-geometry design system</li> <li>• Higher cost primary coolant</li> <li>• Higher cost for well-suited material</li> </ul>

### V. WASTE MANAGEMENT

Nuclear waste is the element that are potential effects on the public assumption of nuclear strength so the next-generation

reactor could have a significant technological system for dealing with the treatment of high-level waste [23]. There are two main constituents of high-level radioactive waste which are; (1) fission products generated in the process of fission and (2) transuranic elements or actinides, which are formed by

neutron capture as a result. Actinides dominate on a long-term basis from a radiological danger point of view. The relative radiological risk factors are depicted in Fig. 5 about fission products and actinides for spent fuel LWR, Fission output decay to enough low level over a few hundred years that their radiological chance factor left below the cancer risk stage of the initial uranium ore [24]. On the other side, Actinides usually have long half-lives, and their radiological danger factor for tens or a huge number of years remains significant degrees greater than that attributed to fission products. Therefore, it will be affirmed as a good motivation to split actinides and rearrange them back into the in-situ burning reactor. The separation of actinides has two distinct advantages in IFR pyro processing from the flow of waste [25]. First of all, in the IFR phase, most of the actinides follow the uranium/plutonium product stream and the residual actinides could be isolated more easily from the waste streams than in the PUREX phase. For burning actinide, the hardened IFR neutron spectrum is reliable than that of any other level of the reactor. Therefore, the IFR concept's ability to make reuse of actinide feasible is very exciting.

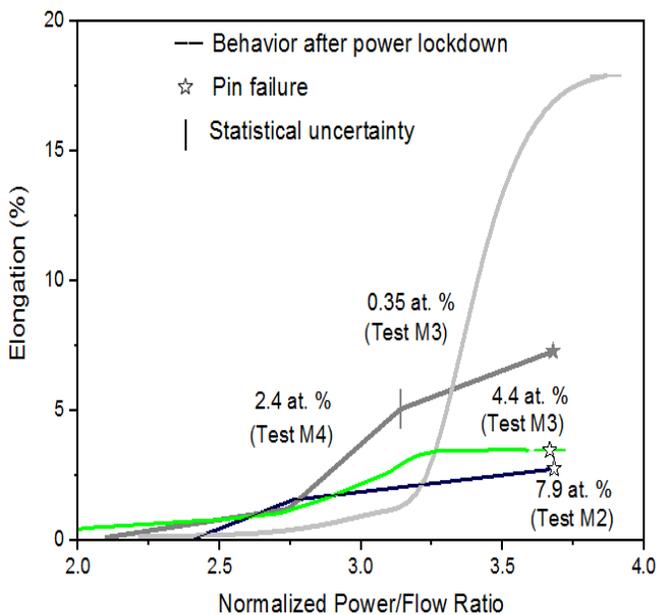


Figure 5 Fission gas carrier axial elongation of metallic fuel under transient overpower conditions simulated in treated tests.

## VI. CONCLUSION

This research article mainly focused on the IFR concept by using the safety passive inherent approach and EBR-II. The IFR has a proud history owing to its feasibility. The safety passive inherent approach was carried which helps the IFR to maintain its cost-effectiveness. The safety passive inherent approach assists the reactor to shut down safely. It has the attaining capacity feature which is similar to the best commercial operating plants. Additionally, it is proved that the EBR-II has contributed greatly to the development of the IFR design, passive inherent safety, materials, fuel development, and the reprocessing of the IFR. Hence, each of the research linked with the IFR development for many decades depends on some approach on the detailed gate from the EBR-II. Hence, it can be affirmed that the IFR concept by using passive inherent safety, materials, fuel development, and the reprocessing of the IFR.

Hence, each of the research linked with the IFR development for many decades depends on some approach on the detailed gate from the EBR-II. Hence, it can be affirmed that the IFR concept by using passive inherent safety, economics, and waste management can be an efficient approach for future development and research directions.

## VII. ACKNOWLEDGMENT

This research work was funded by the Natural Science Foundation of Heilongjiang Province, China (Grant No. A2016002), the Foundation of Science and Technology on Reactor System Design Technology Laboratory (HT-KFKT-14-2017003), the technical support project for Suzhou Nuclear Power Research Institute (SNPI) (No.029-GN-B-2018-C45-P.0.99-000 03) and the Research Institute of Nuclear Power Operation (No. RIN180149-SCCG).

## VIII. REFERENCES

- [1]. Walters, L.C., Thirty years of fuels and materials information from EBR-II. *Journal of Nuclear Materials* 270, 1998: p. 39-88.
- [2]. Kwi Lim Lee, K.S.H., Jae Jeong, Chi Woong Choi, Taekyeong Jeong, Sang June Ahn, Seung Won Lee, Won Pyo Chang, Seok Hun Kang, and Jaewoon Yoo, A Preliminary Safety Analysis For the Prototype Gen IV Sodium Cooled Fast Reactor. *Nuclear Engineering and Technology*, 2016: p. 1071-1082.
- [3]. Chang, Y.I., The Integral Fast Reactor. *Nuclear Technology*, 2017. **88**(2): p. 129-138.
- [4]. Sofu, T., A Review of Inherent Safety Characteristics of Metal Alloy Sodium-Cooled Fast Reactor Fuel Against Postulated Accidents. *Nuclear Engineering and Technology*, 2015: p. 227-239.
- [5]. Zeyun wu, C.I., Sarah Morgan, Sama Bilbao y Leon, and Matthew Bucknor, A status review on the thermal stratification modeling methods for Sodium-cooled Fast Reactors. *Progress in Nuclear Energy*, 2020. **125**.
- [6]. Pope, M.A., et al., Thermal hydraulic challenges of Gas Cooled Fast Reactors with passive safety features. *Nuclear Engineering and Design*, 2009. **239**(5): p. 840-854.
- [7]. Idaho, EBR-II Sixteen year of Operation. 1980: Argonne National Laboratory-West. p. 1-83.
- [8]. A Rineiskii, W.M., A Badulescu, and YI Kim, Liquid Metal Cooled Reactors Experience in Design and Operation. 2007, IAEA: Austria. p. 1-63.
- [9]. DL Porter, H.M.C., PG Medvedev, SL Hayes, and MC Teague, Performance of Low Smear Density Sodium-Cooled Fast Reactor Metal Fuel. *Journal of Nuclear Materials*, 2015: p. 1-25.
- [10]. Takeda, T., et al., Effect of void propagation to sodium void reactivity in transient analyses of fast reactors with sodium-plenum. *Annals of Nuclear Energy*, 2018. **119**: p. 175-179.
- [11]. AS Bochkarev, P.A., AS Korsun, and VS Kharitonov, Modeling of Natural Circulation for the Inherent Safety Analysis of Sodium Cooled Fast Reactors.

- Nuclear Engineering and Technology, 2016: p. 294-298.
- [12]. JI Xing, D.S., and Yuxiang Wu, HPR1000 Advanced Pressurized Water Reactor with Active and Passive Safety. Engineering, 2016: p. 79-87.
- [13]. Petrovic, L.H.B., Development of Methodology for Efficient Fuel Design Evaluation of the Advanced High Temperature Reactor (AHTR). Annals of Nuclear Energy, 2018: p. 646-660.
- [14]. F Khoshahval, A.Z., H Minuchehri, and M Sadighi, and A Norouzi, PWR Fuel Management Optimization using Continuous Particle Swarm Intelligence. Annals of Nuclear Energy, 2010: p. 1263-1271.
- [15]. Chang, D.C.W.Y.I., The Integral Fast Reactor Concept: Physics of Operation and Safety. Nuclear Science and Engineering, 2017. **100**(4): p. 507-524.
- [16]. Jaewoon Yoo, J.C., JaeYong Lim, JinSik Cheon, TaeHo Lee, SungKyun Kim, Kwi LimLee, and Hyung Kook Joo, Overall System Description and Safety Characteristics of Prototype Gen IV Sodium Cooled Fast Reactor in Korea. Nuclear Engineering and Technology, 2016: p. 1059-1070.
- [17]. Zhang You Peng, W., Janne Gu, Long Yang, Sheng Zhao , Jin Yang li, and Tian ji peng Axial expansion for prompt safety of a small lead-cooled reactor. Annals of Nuclear Energy, 2020. **147**.
- [18]. Scott Middlemas, Z.H., Vinay Chauhan, WTanner Yorgason, Robert Schley, Amey Khanolkar, Marat Khafizov, and Dvid Hurley, Determining Local Thermal Transport in a Composite Uranium-Nitride Silicide Nuclear Fuel using Square-pluse Transient Thermorelectance Technique. Journal of Nuclear Materials, 2020: p. 1-11.
- [19]. Hartanto, D., et al., Impacts of Burnup-Dependent Swelling of Metallic Fuel on the Performance of a Compact Breed-and-Burn Fast Reactor. Nuclear Engineering and Technology, 2016. **48**(2): p. 330-338.
- [20]. W Barry Brook, J.B.V.E., Daniel A Meneley, and Thomas A Bles, The Case for a Near-Term Commerical Demonstration of the Interl Fast Reactor. Sustainable Materials and Technologies, 2015: p. 2-6.
- [21]. Benito Mignacca, a.G.L., Economics and Finance of Molten Salt Reactors. Progress in Nuclear Energy, 2020: p. 1-12.
- [22]. Haihua Zhao, H.Z., Vincent AMousseau, and Per FPeterson, Improving SFR Economics Through Innovation from Thermal Design and Analysis Aspect. Nuclear Engineering and Design, 2009: p. 1042-1055.
- [23]. M Salvatores, A.Z., C Girard, M Delpech, I Sleearov, and Tommasi, Nuclear Waste Transmutation. pergamon, 1995: p. 681-687.
- [24]. Jason, Setting the Scene. 1995, UK: The Evolution of the Current Organisational Arrangments in the UK. p. 1-21.
- [25]. DE Holcomb, G.F., BW Patton, JC Gehin, RL Howard, and TJ Harrison, Fast Spectrum Molten Salt Reactor Options. 2011: US Department of energy. p. 1-30.



Journal of Applied and Emerging Sciences by BUITEMS is licensed under a [Creative Commons Attribution 4.0 International License](https://creativecommons.org/licenses/by/4.0/).